# Liquid-liquid equilibria for aniline + benzene + *n*-heptane and methanol + aniline + *n*-heptane + benzene at $25^{\circ}$ C

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#### Abstract

Experimental tie-line data have been measured for aniline + benzene + n-heptane and methanol + aniline + n-heptane + benzene at 25°C. The experimental results have been satisfactorily correlated with the modified Wilson equation including binary, ternary and quaternary parameters obtained in fitting the equation to published and present experimental data.

LIST OF SYMBOLS

$a_{ij}$	binary	energy	parameter	for <i>i–j</i> pair

- F objective function as defined by eqn. (5)
- *R* universal gas constant
- T absolute temperature
- $V_i$  liquid molar volume of pure component *i*
- $x_i$  liquid mole fraction of component *i*

# Greek letters

$\alpha_{ij}$	binary parameter in modified Wilson model for $i-j$ pair
γi	activity coefficient of component i
δ	deviations of experimental values from calculated results
$\Lambda_{ij}$	Wilson-like parameter for $i-j$ pair
$\Lambda_{iki}, \Lambda_{ikli}$	modified Wilson ternary and quaternary parameters

## **Subscripts**

calc	calculated
exptl	experimental
i, j, k, l	components

#### INTRODUCTION

As part of continuing studies on the measurements of liquid-liquid equilibria (LLE) of ternary and quaternary systems, this paper reports tie-lines for aniline + benzene + *n*-heptane and methanol + aniline + *n*-heptane + benzene at 25°C. The experimental results have been well correlated with those calculated from the modified Wilson models having binary, ternary, and quaternary parameters [1, 2]. Binary energy parameters are available for the following systems: methanol + aniline at 20°C [3]; methanol + benzene at 35°C [4]; aniline + benzene at 25°C [5]; *n*-heptane + benzene at 45°C [6]; methanol + *n*-heptane at 25°C [1]. Ternary tie-lines at 25°C have been reported for the methanol + aniline + *n*-heptane [7] and methanol + benzene + *n*-heptane systems [8].

#### **EXPERIMENTAL**

Aniline (Kanto Chemical Co. Inc., special grade) and *n*-heptane (Kanto Chemical Co. Inc., spectro-analysis grade) were used without further purification. Methanol (Wako Pure Chemical Industries Ltd., first grade) was subjected to fractional distillation after shaking with calcium oxide. Benzene (Kanto Chemical Co. Inc., first grade) was purified by repeated fractional recrystallization. The densities of these chemicals, measured with an Anton Paar densimeter (DMA40) at  $25^{\circ}$ C, were in excellent agreement with published values [9] as shown in Table 1.

Tie-line measurements were carried out as described previously [10]. The compositions of two liquids in equilibrium were determined by combining use of a Shimadzu gas chromatograph (GC-8C) and a Shimadzu Chromatopac (C-R3A). The experimental error of measured mole fractions was at most 0.002.

Tables 2 and 3 give the experimental tie-line values of the ternary aniline + benzene + n-heptane and quaternary methanol + aniline + n-heptane + benzene systems at 25°C.

Component	Density/g mol <sup>-1</sup>			
	Obs.	Lit. [9]		
Aniline	1.01746	1.01750		
Methanol	0.78668	0.78637		
Benzene	0.87371	0.87360		
<i>n</i> -Heptane	0.67953	0.67946		

TABLE 1

Densities of pure components at 25°C

## TABLE 2

Experimental tie-line values for aniline(1) + benzene(2) + n-heptane(3) at 25°C

Phase I			Phase II			
$\overline{x_1}$	<i>x</i> <sub>2</sub>	<i>x</i> <sub>3</sub>	<i>x</i> <sub>1</sub>	<i>x</i> <sub>2</sub>	<i>x</i> <sub>3</sub>	
0.1116	0.0628	0.8256	0.8820	0.0493	0.0687	
0.1473	0.1154	0.7373	0.8110	0.1066	0.0824	
0.1812	0.1750	0.6438	0.7387	0.1484	0.1129	
0.2172	0.2014	0.5814	0.6878	0.1769	0.1353	
0.3161	0.2451	0.4388	0.5648	0.2265	0.2087	

### TABLE 3

Experimental tie-line values for methanol(1) + aniline(2) + *n*-heptane(3) + benzene(4) obtained by mixing pure *n*-heptane and benzene with  $\{x'_1 \text{ methanol} + (1 - x'_1) \text{ aniline}\}$  at 25°C

Phase I			Phase II				
<i>x</i> <sub>1</sub>	<i>x</i> <sub>2</sub>	<i>x</i> <sub>3</sub>	x <sub>4</sub>	$x_1$	<i>x</i> <sub>2</sub>	<i>x</i> <sub>3</sub>	<i>x</i> <sub>4</sub>
$x'_1 = 0.75$							
0.1114	0.0568	0.7807	0.0511	0.6678	0.2095	0.0975	0.0252
0.1513	0.0685	0.6876	0.0926	0.6260	0.2062	0.1173	0.0505
0.1900	0.0780	0.6134	0.1186	0.6033	0.1873	0.1393	0.0698
0.2221	0.0935	0.5520	0.1324	0.5671	0.1869	0.1606	0.0854
0.2492	0.0957	0.5153	0.1398	0.5540	0.1745	0.1762	0.0953
$x'_1 = 0.50$	I						
0.0602	0.0834	0.8017	0.0547	0.4405	0.4567	0.0727	0.0301
0.0838	0.1150	0.6483	0.1229	0.4029	0.4154	0.1016	0.0801
0.0997	0.1383	0.6081	0.1539	0.3755	0.3918	0.1283	0.1044
0.1293	0.1645	0.5342	0.1720	0.3535	0.3670	0.1526	0.1267
0.1495	0.1750	0.4953	0.1802	0.3319	0.3439	0.1842	0.1400
$x'_1 = 0.25$	i						
0.0155	0.0839	0.8497	0.0507	0.2074	0.6970	0.0627	0.0329
0.0262	0.1224	0.7265	0.1249	0.1929	0.6338	0.0853	0.0880
0.0407	0.1720	0.6129	0.1744	0.1776	0.5788	0.1114	0.1322
0.0516	0.2213	0.5279	0.1992	0.1670	0.5389	0.1328	0.1613
0.0654	0.2457	0.4730	0.2159	0.1388	0.4786	0.1960	0.1866

# ANALYSIS OF EXPERIMENTAL RESULTS

The experimental tie-line results have been correlated using the modified Wilson equation having binary, ternary and quaternary parameters [2]. The

modified Wilson equation gives the activity coefficient of component 1 in a quaternary mixture

$$\ln \gamma_{1} = -\ln \left[ \left( \sum_{j}^{4} \alpha_{1j} \Lambda_{1j} x_{j} + \Lambda_{231} x_{2} x_{3} + \Lambda_{241} x_{2} x_{4} + \Lambda_{341} x_{3} x_{4} + \Lambda_{2341} x_{2} x_{3} x_{4} \right) \left/ \sum_{j}^{4} \alpha_{1j} x_{j} \right] \\ - x_{1} \left( \frac{1 - \Lambda_{231} x_{2} x_{3} - \Lambda_{241} x_{2} x_{4} - \Lambda_{341} x_{3} x_{4} - 2\Lambda_{2341} x_{2} x_{3} x_{4}}{\sum_{j}^{4} \alpha_{1,j} \Lambda_{1j} x_{j} + \Lambda_{231} x_{2} x_{3} + \Lambda_{241} x_{2} x_{4} + \Lambda_{341} x_{3} x_{4} + \Lambda_{2341} x_{2} x_{3} x_{4}} - \frac{\alpha_{11}}{\sum_{j}^{4} \alpha_{1,j} x_{j}} \right) \\ - x_{2} \left[ \frac{\alpha_{21} \Lambda_{21} + \Lambda_{132} x_{3} (1 - x_{1}) + \Lambda_{142} x_{4} (1 - x_{1}) - \Lambda_{342} x_{3} x_{4} + \Lambda_{1342} x_{1} x_{3} x_{4} (1 - 2x_{1})}{\sum_{j}^{4} \alpha_{2j} \Lambda_{2j} x_{j} + \Lambda_{132} x_{1} x_{3} + \Lambda_{142} x_{1} x_{4} + \Lambda_{342} x_{3} x_{4} + \Lambda_{1342} x_{1} x_{3} x_{4}} - \frac{\alpha_{21}}{\sum_{j}^{4} \alpha_{2j} x_{j}} \right] \\ - x_{3} \left[ \frac{\alpha_{31} \Lambda_{31} + \Lambda_{123} x_{2} (1 - x_{1}) + \Lambda_{143} x_{4} (1 - x_{1}) - \Lambda_{243} x_{2} x_{4} + \Lambda_{1243} x_{1} x_{2} x_{4}}{\sum_{j}^{4} \alpha_{3j} \Lambda_{3j} x_{j} + \Lambda_{123} x_{1} x_{2} + \Lambda_{143} x_{1} x_{4} + \Lambda_{243} x_{2} x_{4} + \Lambda_{1243} x_{1} x_{2} x_{4}} - \frac{\alpha_{31}}{\sum_{j}^{4} \alpha_{3j} x_{j}} \right] \\ - x_{4} \left[ \frac{\alpha_{41} \Lambda_{41} + \Lambda_{124} x_{2} (1 - x_{1}) + \Lambda_{134} x_{3} (1 - x_{1}) - \Lambda_{234} x_{2} x_{3} + \Lambda_{1234} x_{1} x_{2} x_{3}}{\sum_{j}^{4} \alpha_{4j} \Lambda_{4j} x_{j} + \Lambda_{124} x_{1} x_{2} + \Lambda_{134} x_{1} x_{3} + \Lambda_{234} x_{2} x_{3} + \Lambda_{1234} x_{1} x_{2} x_{3}} \right]$$

where  $\alpha_{ij}$  and  $\Lambda_{ij}$  are the binary parameters. The values of  $\alpha_{ij}$  are unity for completely miscible mixtures and are empirically assigned values, which are slightly larger than unity, for partially miscible mixtures.  $\Lambda_{ii}$  is defined by

$$\Lambda_{ij} = (V_j / V_i) \exp(-a_{ij} / T)$$
<sup>(2)</sup>

 $\Lambda_{jki(i \neq j \neq k)}$  and  $\Lambda_{jkli(i \neq j \neq k \neq l)}$  are also the ternary and quaternary parameters to be determined from the experimental tie-line results.

The expressions of  $\ln \gamma_2$ ,  $\ln \gamma_3$  and  $\ln \gamma_4$  are obtained successively by cyclic advancement of the subscripts in eqn. (1) by changing 1 to 2, 2 to 3, 3 to 4, and 4 to 1.

Table 4 shows the binary Wilson-like parameters. The values of the energy parmeters  $a_{ii}$  for partially miscible mixtures were obtained by solving

System (1 + 2)	Temp./ °C	Parameters				
		$a_{12}/{ m K}$	$a_{21}/K$	$\alpha_{12}$	$\alpha_{21}$	
Aniline + benzene	25	269.28	9.08	1.0	1.0	
Aniline $+ n$ -heptane	25	979.99	797.62	1.1	1.1	
<i>n</i> -Heptane- + benzene	45	216.55	55.20	1.0	1.0	
Methanol + aniline	20	338.35	- 52.29	1.0	1.0	
Methanol + benzene	35	889.85	92.17	1.0	1.0	
Methanol $+ n$ -heptane	25	1158.4	552.61	1.0	1.1	

Binary Wilson-like parameters

TABLE 4

the thermodynamic equation (eqn. (3)) for each component at two equilibrated liquid phases I and II and satisfying simultaneously eqn. (4).

$$(x_i \gamma_i)^{\mathrm{I}} = (x_i \gamma_i)^{\mathrm{II}}$$
(3)

$$\sum_{i} x_{i}^{\mathrm{I}} = 1 \qquad \text{and} \qquad \sum_{i} x_{i}^{\mathrm{II}} = 1 \tag{4}$$

The ternary parameters of the modified Wilson equation were obtained by minimizing the following objective function with a simplex method [11].

$$F = \left[\sum_{i} \sum_{j} \sum_{k} (x_{ijk, \text{ calc}} - x_{ijk, \text{ expt1}})^2 / 6M\right]^{0.5}$$
(5)

where i = 1, 2, 3 (components), j = 1, 2 (phases) and k = 1, 2, ..., M (tielines). Table 5 gives the ternary calculated results. Figure 1 shows the experimental tie-lines and the calculated results for the three ternary systems. Table 6 gives also the quaternary calculated results and Table 7 shows

#### TABLE 5

The results of fitting the modified Wilson equation to ternary tie-lines at 25°C

System (1 + 2 + 3)	Туре	Number of data points	Ternary parameters	F/mol%
Aniline + benzene + <i>n</i> -heptane	I	5	$\begin{array}{ccc} \Lambda_{231} & 0.0653 \\ \Lambda_{132} & -0.0237 \\ \Lambda_{123} & -0.1809 \end{array}$	0.36
Methanol + aniline + <i>n</i> -heptane	II	9	$\begin{array}{ccc} \Lambda_{231} & 0.0728 \\ \Lambda_{132} & -0.3346 \\ \Lambda_{123} & 0.0658 \end{array}$	0.59
Methanol + benzene + <i>n</i> -heptane	Ι	8	$\begin{array}{ccc} \Lambda_{231} & 0.1746 \\ \Lambda_{132} & 0.1967 \\ \Lambda_{123} & 0.0823 \end{array}$	0.44

## TABLE 6

The results of fitting the modified Wilson equation to the quaternary tie-line results at 25°C

System $(1 + 2 + 3 + 4)$	No. of data points	Quaternary parameters	Deviations/mol%		
			AAM <sup>a</sup>	RMS <sup>b</sup>	
Methanol + aniline + n-heptane +	15	$\begin{array}{rrrr} \Lambda_{2341} & -0.0430 \\ \Lambda_{1342} & 0.0923 \\ \Lambda_{1234} & -1.5948 \end{array}$	0.87 1.86 °	0.98 2.27 °	
benzene		$\Lambda_{1234}$ 3.6738			

<sup>a</sup> AAM, absolute arithmetic mean deviation. <sup>b</sup> RMS, root-mean-squared deviation. <sup>c</sup> Predicted value based on the binary and ternary parameters.



Fig. 1. Calculated liquid-liquid equilibria for three ternary systems at  $25^{\circ}$ C:  $\bigcirc - \cdot - \cdot - \bigcirc$ , experimental tie line; —, calculated from the modified Wilson equation with binary and ternary parameters. A, Aniline + methanol + *n*-heptane [7]; B, aniline + benzene + *n*-heptane, this work; C, methanol + benzene + *n*-heptane [8].

	Phase I		Phase II		
	AAM <sup>a</sup>	RMS <sup>b</sup>	AAM	RMS	
$\delta x_1$	0.0117	0.0131	0.0122	0.0127	
$\delta x_2$	0.0114	0.0129	0.0125	0.0137	
$\delta x_3$	0.0115	0.0127	0.0056	0.0077	
$\delta x_4$	0.0026	0.0030	0.0024	0.0027	

Detailed calculated results for methanol(1) + aniline(2) + $n$ -heptane(3) + benzene(4) at 25°	°C
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<sup>a</sup> AAM, absolute arithmetic mean deviation between the experimental and calculated liquid mole fractions. <sup>b</sup> RMS, root-mean-squared deviation between the experimental and calculated liquid mole fractions.

the detailed deviations between the experimental and calculated liquid mole fractions.

We may conclude that the experimental tie-line results for the ternary and quaternary systems studied here have been well correlated with the modified Wilson equation having binary, ternary and quaternary parameters.

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TABLE 7

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